

Namelist options in FV³

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6 March 2017

FV³ Documentation

Proposed NCEP Office Note 472 (?) for
distribution with public code release

Draft in limited distribution

Comprehensive document describing
solver algorithm, configuration, and
usage

Focusing on solver and diffusion options
in this presentation; see document for
complete coverage

FV³: THE GFDL FINITE-VOLUME CUBED-SPHERE DYNAMICAL CORE

The GFDL FV³ Team

March 5, 2017

NCEP Office Note 472 (Proposed) (**DRAFT, unfinished**)
Not for distribution beyond
GFDL, GSFC, EMC, CAPS, PSD, AOML
Contact GFDL FV³ support
(oar.gfdl.fvGFS_support@noaa.gov) if found elsewhere

FV³ namelist options

&fv_core_nml

npx = 769
npy = 769
npz = 63
n_sponge = 8
tau = 5.
rf_cutoff = 8.e2
d2_bg_k1 = 0.16
d2_bg_k2 = 0.02
hydrostatic = .F.
k_split = 2
n_split = 6
fv_sg_adj = 1800
nord = 2
d4_bg = 0.15
vtdm4 = 0.
do_vort_damp

= .false.

d_con = 0.
hord_mt = 8
hord_vt = 8
hord_tm = 8
hord_dp = 8
hord_tr = 8

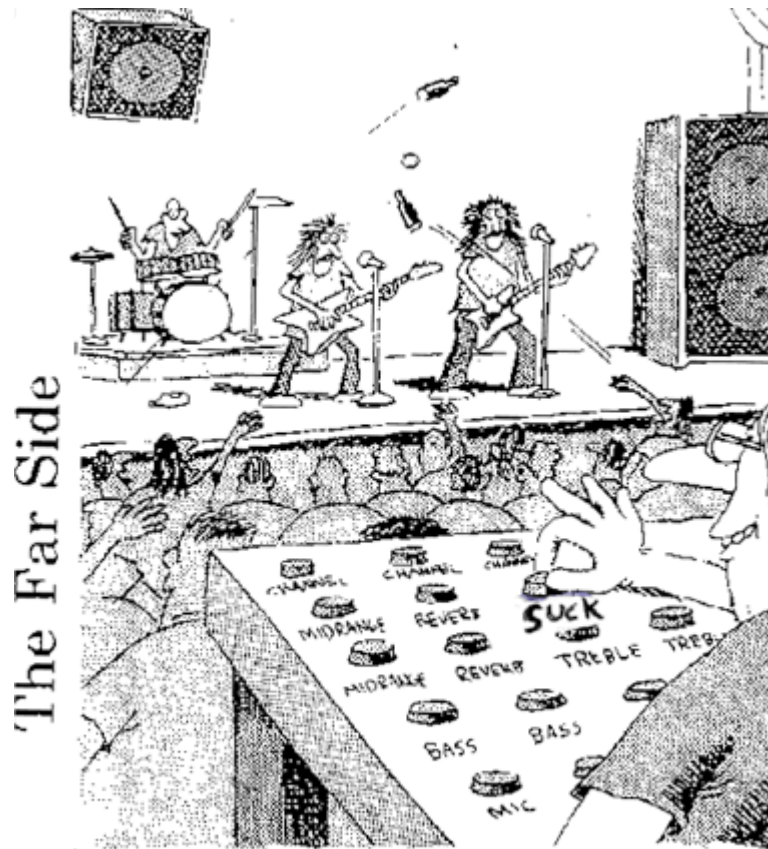
Describing key parameters in a sample configuration used for 13-km forecasts, configured for Zhao-Carr microphysics

Some parameters (hord_xx) will be updated for public release NEMS and CM4 versions; changes in behavior will be noted below

WARNING

If you don't know what an option does, don't mess with it

Unfortunately no
`do_what_I_want = .true.` option



Raymond's last day as the band's sound technician.

Domain specification

&fv_core_nml

npx = 769
npv = 769
npz = 63
n_sponge = 8
tau = 5.
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d2_bg_k1 = 0.16
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hord_tr = 8

npx and npv control the number of grid corners across a cube face; subtract one to get the number of grid cells

c768 corresponds roughly to $\frac{1}{8}$ degree, or 12 km global average grid-cell width

On the global grid npx = npv
But they can differ on a nest

npz is the number of grid levels, with a hard-coded specification of level placement

64-level model top at ~0.6 mb

Good configurations are nontrivial to design

Domain specification

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npx = 769

npv = 769

npz = 63

n_sponge = 8

tau = 5.

rf_cutoff = 8.e2

d2_bg_k1 = 0.16

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fv_sg_adj = 1800

nord = 2

d4_bg = 0.15

vtdm4 = 0.

do_vort_damp

= .false.

d_con = 0.

hord_mt = 8

hord_vt = 8

hord_tm = 8

hord_dp = 8

hord_tr = 8

npz is the number of grid levels, with a hard-coded specification of level placement

63-level model top at constant 0.6 mb pressure

Good configurations are nontrivial to design

Enhanced resolution in PBL (and possibly UTLS)

Smooth variation in pressure levels

Choose a good model top

Timestepping

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hydrostatic = .F.
k_split = 2
n_split = 6
fv_sg_adj = 1800
nord = 2
d4_bg = 0.15
vtdm4 = 0.
do_vort_damp = .false.
d_con = 0.
hord_mt = 8
hord_vt = 8
hord_tm = 8
hord_dp = 8
hord_tr = 8

&coupler_nml

dt_atmos = 225

dt_atmos is the physics timestep: **225 s**, matching GFS

Physics is applied forward-in-time, consistent

with

FV³ dynamics

Vertical remapping is done k_split times per
physics timestep

112.5 s: Lagrangian vertical coordinate has *no*
Courant number restriction!

k_split > 1 can enhance stability for the same
acoustic timestep, with a minimal performance
degradation

Timestepping

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d2_bg_k1 = 0.16
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hydrostatic = .F.
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n_split = 6
fv_sg_adj = 1800
nord = 2
d4_bg = 0.15
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hord_vt = 8
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&coupler_nml

dt_atmos = 225

Acoustic solver and horizontal dynamics called n_split times between vertical remappings

Dynamics advanced by forward-backward timestepping, with sub-cycled tracer advection

Acoustic timestep = $dt_{atmos} / k_split * n_split$

18.75 s in this example

Monotonic scheme

```
&fv_core_nml
  npx          = 769
  npy          = 769
  npz          = 63
  n_sponge = 8
  tau = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 2
  d4_bg = 0.15
  vtdm4 = 0.
  do_vort_damp = .false.
  d_con = 0.
  hord_mt = 8
  hord_vt = 8
  hord_tm = 8
  hord_dp = 8
  hord_tr = 8
```

Non-monotonic ("linear") scheme

```
&fv_core_nml
  npx          = 769
  npy          = 769
  npz          = 63
  n_sponge = 8
  tau = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 2
  d4_bg = 0.15
  vtdm4 = 0.04
  do_vort_damp = .true.
  d_con = 1.
  hord_mt = 5
  hord_vt = 5
  hord_tm = 5
  hord_dp = 5
  hord_tr = 8
```

Optimized monotonic and non-monotonic ("linear") schemes for computing fluxes. Tracer advection is *always* monotonic (8; -8 in NGGPS code) and is *never* explicitly diffused

Monotonic scheme (8; -8 in NGGPS code) is intrinsically diffusive to 2-delta-waves. Explicit horizontal damping from 6th-order (nord = 2) divergence damping

No explicit ("vorticity") damping on other fluxes

`do_vort_damp = .false.`

Monotonic scheme

&fv_core_nml

npx = 769
npy = 769
npz = 63
n_sponge = 8
tau = 5.
rf_cutoff = 8.e2
d2_bg_k1 = 0.16
d2_bg_k2 = 0.02
hydrostatic = .F.
k_split = 2
n_split = 6
fv_sg_adj = 1800
nord = 2
d4_bg = 0.15
vtdm4 = 0.
do_vort_damp = .false.
d_con = 0.
hord_mt = 8
hord_vt = 8
hord_tm = 8
hord_dp = 8
hord_tr = 8

Non-monotonic ("linear") scheme

&fv_core_nml

npx = 769
npy = 769
npz = 63
n_sponge = 8
tau = 5.
rf_cutoff = 8.e2
d2_bg_k1 = 0.16
d2_bg_k2 = 0.02
hydrostatic = .F.
k_split = 2
n_split = 6
fv_sg_adj = 1800
nord = 2
d4_bg = 0.15
vtdm4 = 0.04
do_vort_damp = .true.
d_con = 1.
hord_mt = 5
hord_vt = 5
hord_tm = 5
hord_dp = 5
hord_tr = 8

Non-monotonic scheme (5; 6/-5 in NGGPS code) applies *no* monotonicity constraint ("linear", "unlimited"), only a 2dx filter to suppress oscillations.

Needs consistent damping to vorticity and other fluxes. This damping (vtdm4) should be weaker than the divergence damping.

Artificial diffusion

```
&fv_core_nml
  npz = 63
  npy = 769
  npz = 63
  n_sponge = 8
  tau = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 2
  d4_bg = 0.15
  vtdm4 = 0.04
  do_vort_damp
= .true.

  d_con = 1.
  hord_mt = 5
  hord_vt = 5
  hord_tm = 5
  hord_dp = 5
  hord_tr = 8
```

Explicit divergence damping necessary since there is no implicit diffusion to divergence

Strength d4_bg should range from 0.10 to 0.16

All damping applied **along** Lagrangian surfaces

Optional damping to other fluxes (vorticity, air mass, w, θ) controlled by vtdm4 “vorticity damping”

Strongly recommended if non-mono scheme is used

Vortical and divergent modes damped separately. vtdm4 should be much smaller than d4_bg

Artificial diffusion

&fv_core_nml

npx = 769
npy = 769
npz = 63
n_sponge = 8
tau = 5.
rf_cutoff = 8.e2
d2_bg_k1 = 0.16
d2_bg_k2 = 0.02
hydrostatic = .F.
k_split = 2
n_split = 6
fv_sg_adj = 1800
nord = 2
d4_bg = 0.15
vtdm4 = 0.04
do_vort_damp

d_con = 1.
hord_mt = 5
hord_vt = 5
hord_tm = 5
hord_dp = 5
hord_tr = 8

= .true.

The local dissipated kinetic energy from flux damping can be added back as heat ($d_con = 1$) for better conservation of lost energy

Can cause instability if vtdm4 is small

Set d_con to 0 if $vtdm4 < 0.02$

Damping order is $2 \times (nord+1)$; fourth, sixth, and eighth-order scale-selective damping are available

Rayleigh damping and sponge layer

&fv_core_nml

npx = 769

npz = 769

npz = 63

n_sponge = 8

tau = 5.

rf_cutoff = 8.e2

d2_bg_k1 = 0.16

d2_bg_k2 = 0.02

hydrostatic = .F.

k_split = 2

n_split = 6

fv_sg_adj = 1800

nord = 2

d4_bg = 0.15

vtdm4 = 0.

do_vort_damp = .false.

d_con = 0.

hord_mt = 8

hord_vt = 8

hord_tm = 8

hord_dp = 8

hord_tr = 8

Rayleigh damping is applied *consistently* to (u, v, w) with timescale tau (here 5 days)

Lost kinetic energy converted to heat

Rayleigh damping is only applied above rf_cutoff (in Pa); the top 6 layers in this case

Should be tuned with GWD to produce the most stable and noise-free result

Consider more sponge layers with weaker damping (larger tau)

Rayleigh damping and sponge layer

&fv_core_nml

npx = 769

npz = 769

npz = 63

n_sponge = 8

tau = 5.

rf_cutoff = 8.e2

d2_bg_k1 = 0.16

d2_bg_k2 = 0.02

hydrostatic = .F.

k_split = 2

n_split = 6

fv_sg_adj = 1800

nord = 2

d4_bg = 0.15

vtm4 = 0.

do_vort_damp = .false.

d_con = 0.

hord_mt = 8

hord_vt = 8

hord_tm = 8

hord_dp = 8

hord_tr = 8

Sponge layer is active in the top two layers of the model, using second-order horizontal damping to suppress wave reflection

d2_bg_k1 should be between 0.16 and 0.2

d2_bg_k2 should be much smaller

A 2dz filter controls local dynamic instability in top n_sponge layers only

Relaxes $Ri < 1$ nonlinear instabilities with timescale fv_sg_adj

Diffusion and damping

Well-configured numerical diffusion, damping, sponge layers, and GWD can greatly improve the stability of the model.

Decreasing the timestep should be a last resort:

consider re-tuning diffusion first

Keeping forecast skill and quality in mind, of course

Damping and timestep length are physics-dependent. Different drag schemes and prognostic microphysics may require different damping and timesteps.

Physics and dynamics need to be optimized together.

Other options of interest

`kord_{tm,mt,wz,tr}` control cubic-spline vertical remapping scheme.

`kord_tm < 0` remaps T , which is much more accurate than remapping θ

`kord_xx = 9` is monotonic, while 10 is non-monotonic with 2dz filter on spline.

11 is non-monotonic with no filter

`dddmp` is the coefficient for 2D nonlinear Smagorinsky damping, which is more flow-dependent than linear damping. Values of 0.1 or 0.2 are recommended.

`nwat`, `dnats`, and `z_tracer` will be very useful when implementing advanced microphysics; ask us for advice

Other options of interest

`consv_te` controls amount of energy lost by solver which is restored by energy fixer (global grid only). AM4 uses 0.6 to reduce imbalance to < 0.01 in AMIP runs.

`print_freq` controls stdout diagnostics:

frequency (hr) if > 0 ; period (# of `dt_atmos`) if < 0

`range_warn`, `fv_debug`, and `no_dycore` are very useful debugging tools controlling checking of invalid values, printing out many more diagnostics, and running the model in column-physics mode

Stretched grid configuration

```
&fv_core_nml
    npx          = 769
    npy          = 769
    npz          = 63
    ....
    nord = 1
    d4_bg = 0.12
    ...
do_schmidt = .true.
target_lat = 35.5
target_lon = -97.5
stretch_fac = 3.0
```

Grid stretching allows simple, easy local grid refinement within a single global grid.

Enable stretching with `do_schmidt = .T.`

Set region center with `target_lat` and `target_lon`

Refinement factor given by `stretch_fac > 1.`

Larger values give a smaller high-res region.

Remember to reduce timestep when stretching!

Use fourth-order damping (`nord = 1`) for stretched grid

Nested grid configuration

```
&fv_core_nml ! nested grid
```

```
  npx      = 1729
```

```
  npy      = 1441
```

```
  ntiles   = 1
```

```
  npz      = 63
```

```
  k_split  = 4
```

```
  n_split  = 5
```

```
&nest_nml
```

```
  ngrids = 2
```

```
  nest_pes = $npes_g1,$npes_g2
```

```
  p_split = 1
```

```
/
```

```
&fv_core_nml ! coarse grid
```

```
  npx      = 769
```

```
  npy      = 769
```

```
  npz      = 63
```

```
....
```

```
  do_schmidt = .true.
```

```
  target_lat = 35.5
```

```
  target_lon = -97.5
```

```
  stretch_fac = 1.5
```

Each grid gets a separate, complete
namelist file input.nml, input_nest02.nml

Physics and infrastructure can be
configured separately on each grid

Showing example from c768r15n3---3 km
over CONUS---with GFDL MP

dt_atmos = 90: $\Delta t = 4.5$ sec

Nested grid configuration

```
&fv_core_nml ! nested grid
```

```
  npx      = 1729
```

```
  npy      = 1441
```

```
  ntiles   = 1
```

```
  npz      = 63
```

```
  k_split  = 4
```

```
  n_split  = 5
```

```
&nest_nml
```

```
  ngrids = 2
```

```
  nest_pes = $npes_g1,$npes_g2
```

```
  p_split = 1
```

```
/
```

```
&fv_core_nml ! coarse grid
```

```
  npx      = 769
```

```
  npy      = 769
```

```
  npz      = 63
```

```
  ....
```

```
  do_schmidt = .true.
```

```
  target_lat = 35.5
```

```
  target_lon = -97.5
```

```
  stretch_fac = 1.5
```

Both namelist files need a nest_nml to specify ngrids (currently limited to 2), processors for each grid, and number of BC/two-way updates per physics timestep (p_split; +1 recommended)

Rotate coarse grid to center tile over nested grid, and stretch as desired

Currently both grids need to have same npz (working on “remap BCs” to support differing vertical levels)

Nested grid configuration

&fv_core_nml ! nested grid

```
npx      = 1729  
npy      = 1441  
ntiles   = 1  
npz      = 63  
k_split  = 4  
n_split  = 5  
nord     = 3  
dddmp    = 0.1  
d4_bg    = 0.08  
vtm4     = 0.005  
do_vort_damp = .T.  
d_con    = 0.0  
...  
nested   = .true.  
twowaynest = .true.  
parent_grid_num = 1  
parent_tile = 6  
refinement = 3  
ioffset  = 97  
joffset  = 165  
nestupdate = 7
```

Several new options must be added to enable nested grid. Only npx, npy, ioffset, joffset are widely configurable, and must match values given for initial conditions.

ioffset, joffset control location of first refined coarse grid cell. This is derivable from preproc tool configuration. (Work is being done to simplify nested-grid setup)

Nested grid configuration

&fv_core_nml ! nested grid

npx = 1729

npz = 1441

ntiles = 1

npz = 63

k_split = 4

n_split = 5

nord = 3

dddmp = 0.1

d4_bg = 0.08

vtdm4 = 0.005

do_vort_damp = .T.

d_con = 0.0

...

nested = .true.

twowaynest = .true.

parent_grid_num = 1

parent_tile = 6

refinement = 3

ioffset = 97

joffset = 165

nestupdate = 7

Damping can be greatly reduced on a limited domain (No Himalayas! No Andes!)

Here using 8th order damping (nord = 3) and much reduced divergence and flux damping. d_con has been disabled.

Also using Smagorinsky-like nonlinear horizontal diffusion (dddmp = 0.1)

Zhao-Carr MP will probably need greater diffusion (nord = 2) than shown here